## 35 W LCD Monitor

| Application | Device | Power Output | Input Voltage | Output Voltage | Topology |
| :--- | :--- | :--- | :--- | :--- | :--- |
| LCD Monitor | TOP257EN | 35 W | $90-264$ VAC | 13 V | Flyback |

## Design Highlights

- Low component count, high efficiency
- Delivers 35 W in $50^{\circ} \mathrm{C}$ ambient temperature environments
- EcoSmart ${ }^{\circledR}$ multi-mode technology meets energy efficiency standards
- 0.55 W output power for <1 W input
- No-load power consumption: <200 mW at 230 VAC
- >82\% Full-load efficiency
- Uses new low profile eSIP-7C high-power package that reduces device height and PCB area
- 132 kHz switching frequency minimizes size and cost of power magnetics
- Integrated safety and reliability features
- Accurate, auto-recovering hysteretic thermal shutdown maintains safe PCB temperatures in any condition
- Auto-restart protects against output short circuits and open feedback loops
- Output overvoltage protection (OVP), configurable for latching or self-recovery
- Input undervoltage (UV) protection prevents power-up or power-down output glitches
- Input overvoltage (OV) protection extends line surge limit
- Compliance to EN55022 and CISPR-22 Class B conducted

Figure 1. Schematic of a 35 W LCD Monitor Using TOP257EN.

## Operation

The design schematic in Figure 1 shows an LCD monitor power supply utilizing the TOPSwitch-HX TOP257EN (U1) in a flyback configuration. This supply operates over a wide input range (90 to 264 VAC), delivering a $13 \mathrm{~V}, 35 \mathrm{~W}$ supply to the load.

Y-capacitors C1, C2, and C7 together with inductor L1 provide common mode filtering. Differential mode filtering is provided by X-capacitor C3 and by the bulk capacitor C4. The filtered AC goes to a bridge rectifier. Thermistor RT1 limits the inrush current when AC is applied.

IC U1 turns on when the current into the $V$ pin exceeds $25 \mu \mathrm{~A}$. Resistor R3 sets this input voltage threshold to 100 V DC.

IC U1 regulates the output by adjusting the duty cycle of the PWM controller which drives the integrated switching MOSFET. The controller within U1 uses a multi-mode control scheme which seemlessly transitions between different switching modes to maximize efficiency at any load.


A clamp network formed by D5, C6, R1, and R2 limits U1's drain voltage at turn-off. Fast-recovery diode D5 recovers some of the clamp energy; R1 limits reverse diode currents and dampens high-frequency ringing.

The output of the bias winding is rectified by D6 and filtered by C10. Zener diode VR2 and resistor R5 form a latching output overvoltage protection (OVP) circuit. Increased voltage at the output causes increased voltage across C10. In an overvoltage condition Zener VR2 breaks down and current flows into the V pin of IC U1, initiating a latching shutdown. The shutdown can be either latching or auto-recovering depending on the value of R5.

Diodes D7 and D8 rectify the secondary side output. Low-ESR capacitors (C13, C14) filter the output from D7 and D8. A secondorder filter made up of L3 and C15 provides additional filtering on the output that switching noise across C13 and C14.

Resistors R13 and R14 act as a potential divider to sense the output voltage. U3 drives optocoupler U2 through resistor R11 to provide feedback information to U1's C pin.

## Key Design Points

- Fast-recovery diodes D1 and D3 reduce radiated EMI (by eliminating voltage spikes inherent to regular diode highfrequency turn-off snap, and by not conducting AC line-induced noise). Their placement ensures one of the two conducts in each half cycle.
- Y-capacitor C7 placed across the transformer (T1) isolation barrier reduces conducted EMI. The switching frequency is modulated (jittered) to reduce EMI.

- OVP may be configured for latching (as in this design) or for self recovery (non-latching). For non-latching recovery increase R5 to $5.1 \mathrm{k} \Omega$.
- Resistor R4 and C5 form a snubber network across diode D6. With ferrite bead L2 they reduce high-frequency conducted and radiated EMI.


Figure 3. Conducted EMI with EN55022 B Limits. Input: 230 VAC, Maximum Steady-state Load.

## Transformer Parameters

|  | Core Material | EF25, gapped for ALG of $220 \mathrm{nH/} \mathrm{t}^{2}$ |
| :---: | :---: | :---: |
|  | Bobbin | EF25 10 pins, Horizontal |
|  | Winding Details | First half primary: 29T, \#26 AWG Bias/feedback: 8T $\times 4$, \#30 AWG Secondary: 7T $\times 2$, \#23, TIW Shield: 9T $\times 4$, \#39 AWG Second half primary: 27T, \#26 AWG |
|  | Winding Order | First half primary (2-3), Bias/feedback (5-4), Secondary ( $9,10-7,8$ ), Shield (NC-1), Second half primary (3-1) |
|  | Primary Inductance | $690 \mu \mathrm{H}, \pm 5 \%$ |
|  | Primary Resonant Frequency | 1.8 MHz (minimum) |
|  | Leakage Inductance | $13 \mu \mathrm{H}$ (maximum) |

Table 1. Transformer Parameters. (AWG = American Wire Gauge, TIW = Triple Insulated Wire, NC = No Connection)

Figure 2. No-load Input Power vs Line Voltage.

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